Propagation of a Short GRB Jet in the Ejecta: Jet Launching Delay Time, Jet Structure, and GW170817/GRB 170817A

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Abstract

We perform a series of relativistic magnetohydrodynamic simulations to investigate how a hot magnetic jet propagates within the dynamical ejecta of a binary neutron star merger, focusing on how the jet structure depends on the delay time of jet launching with respect to the merger time, Δt_{iet} . We find that regardless of the jet-launching delay time, a structured jet with an angle-dependent luminosity and Lorentz factor is always formed after the jet breaks out of the ejecta. On the other hand, the jet-launching delay time has an impact on the jet structure. If the jetlaunching delay time is relatively long, e.g., ≥ 0.5 s, the line-of-sight material has a dominant contribution from the cocoon. On the other hand, for a relatively short jet-launching delay time, the jet penetrates through the ejecta early on and develops an angular structure afterward. The line-of-sight ejecta is dominated by the structured jet itself. We discuss the case of GW170817/GRB 170817A within the framework of both long and short jet-launching delay time. In the future, more observations of gravitational-wave/gamma-ray burst associations can help to differentiate between these two scenarios.

Key words: gamma-ray burst: general - magnetohydrodynamics (MHD) - methods: numerical

1. Introduction

Gamma-ray bursts (GRBs) are believed to originate from a relativistic jet launched by a compact central engine, either a black hole (BH) or a rapidly rotating, highly magnetized neutron star (NS). After being launched, the jet propagates through and breaks out of the surrounding material before emitting γ -ray photons at large radii. The jet propagation physics has been investigated by many authors using numerical simulations, both within the context of long GRBs for the envelope of a massive progenitor star (e.g., MacFadyen & Woosley 1999; Aloy et al. 2000; Zhang et al. 2003; Morsony et al. 2007; Mizuta & Aloy 2009; Mizuta & Ioka 2013; Geng et al. 2016; López-Cámara et al. 2016), and within the context of short GRBs for the dynamical ejecta of a binary NS merger (Murguia-Berthier et al. 2014; Nagakura et al. 2014). Relevant analytical studies have also been carried out (Bromberg et al. 2011, 2014). These studies show that the interaction between the jet and the surrounding material produces a hot cocoon surrounding the jet, which in turn helps to collimate the jet.

The coincident detection of a gravitational-wave (GW) event GW170817 (Abbott et al. 2017) and a short GRB 170817A (Goldstein et al. 2017; Zhang et al. 2018) confirms the hypothesis that binary NS mergers are the progenitors of at least some short GRBs. In the literature, a uniform conical jet with a sharp edge (also called a top-hat jet) is usually used to interpret GRB prompt emission and afterglows. However, such a simple model fails to explain the prompt emission data of GRB 170817A (e.g., Granot et al. 2017; Gottlieb et al. 2018; Meng et al. 2018). The brightening of the late-time X-ray/ optical/radio afterglow hints at the existence of a significant energy injection, which was interpreted as either lateral injection from a structured jet (Xiao et al. 2017; Kathirgamaraju et al. 2018; Lamb & Kobayashi 2018; Lamb et al. 2019; Lazzati et al. 2018; Lyman et al. 2018; Troja et al. 2018; Xie

et al. 2018; Ghirlanda et al. 2019; Li et al. 2019; Piro et al. 2019) or radial injection from a stratified cocoon (Kasliwal et al. 2017; Nakar & Piran 2017; Margutti et al. 2018; Mooley et al. 2018b). The detection of "superluminal" motion in the radio afterglow (Mooley et al. 2018a; Ghirlanda et al. 2019) ruled out the later scenario and reinforced the structured jet picture. However, it is unclear whether the line-of-sight material, which moves with a mild Lorentz factor, comes from the cocoon surrounding the central jet or from the wing of the structured jet itself.

Observationally, GRB 170817A is delayed with respect to GW170817 by $\Delta t \sim 1.7$ s. The origin of this delay has not been clarified (Gill et al. 2019; Zhang 2019). Some authors (e.g., Bromberg et al. 2018; Gottlieb et al. 2018) attributed a significant portion of this delay to the delay of jet launching, Δt_{iet} . Under such an assumption, the dynamical ejecta already propagates to a distance of $\sim v_{\rm ej} \Delta t_{\rm jet} \sim 6 \times 10^9 \,{\rm cm} \, (v_{\rm ej}/0.2c)$ $(\Delta t_{\rm jet}/1 \, {\rm s})$ when the jet is launched, where $v_{\rm ej}$ is the average velocity of the dynamical ejecta. The interaction between the jet and this extended ejecta is significant, making a significant cocoon component. The prompt γ -ray emission may be explained as the photospheric emission of the cocoon as the jet breaks out of the ejecta (Lazzati et al. 2017; Nakar et al. 2018). On the other hand, Zhang et al. (2018) pointed out that observationally the delay time $\Delta t \sim 1.7$ s is comparable to the duration of the burst $T_{90} \sim 2$ s, which is consistent with the scenario that both timescales are defined by the same physical quantity $\sim R_{\rm GRB}/\Gamma^2 c$. This suggests that the delay timescale is mostly defined by the time when the jet propagates to the dissipation site at R_{GRB} , which is much greater than the photosphere radius for typical parameters. Within this framework, Δt_{iet} is negligibly small. It is thus interesting to investigate the interaction between the jet and the dynamical



ejecta, considering the effect of Δt_{jet} in general. This is one of the main goals of this Letter.

Within the context of short GRBs, and in particular the GW170817/GRB 170817A association, relativistic hydrodynamical simulations have been performed to explore how the jet power and Lorentz factor vary as a function of the polar angle (e.g., Lazzati et al. 2018; Wu & MacFadyen 2018; Xie et al. 2018). In addition to this, the propagation of a Poyntingflux-dominated jet was presented using relativistic magnetohydrodynamic (RMHD) simulations by Bromberg et al. (2018). Recently, Kathirgamaraju et al. (2019) and Fernández et al. (2019) investigated the jet structure by considering the jetlaunching mechanism from the central engine. The density contributions from the post-merger and dynamical ejecta are not considered in these setups. In all of these previous works, the role of Δt_{iet} was not investigated in detail.

In this Letter, we perform a set of axisymmetric 2.5D RMHD simulations to study the propagation of a hot magnetic short GRB jet through the ejecta and after its breakout. We pay special attention on the role of Δt_{jet} in defining the angular structure of the luminosity and Lorentz factor. The simulation setup is presented in Section 2. The simulation results are presented in Section 3, and their application to GW170817/GRB 170817A is discussed in Section 4. Our findings are summarized in Section 5.

2. Simulation Setup

Numerical simulations of binary NS mergers indicate that about 10^{-4} – 10^{-2} solar masses (M_{\odot}) of NS material, called dynamical ejecta, are ejected during the coalescence (Hotokezaka et al. 2013; Shibata et al. 2017). In our simulation of jet propagation, the setups include a proper description of both the dynamical ejecta and the jet itself, which is given in detail below.

2.1. The Dynamical Ejecta

In previous simulations of jet propagation, the ejecta is usually set up according to an initial condition; i.e., a certain density/velocity profile of the ejecta is already set before the jet launching in the simulation domain. On the other hand, the simulations of binary NS mergers show that essentially all of the ejecta materials are ejected within ~ 15 ms, regardless of the equation of state of the NS (Hotokezaka et al. 2013). Because we are investigating how Δt_{jet} affects jet propagation, we adopt a more realistic treatment by setting the inner boundary condition of the ejecta that lasts for 15 ms, and let the ejecta propagate for Δt_{iet} before the jet is launched. The average velocity of the ejecta, v_{ej} , is assumed to have a typical value $\sim 0.2c$. The density of the ejecta is set to have an angular profile, i.e., denser near the equator and more dilute near the axis. The initial density profile of the ejecta is set to (see Kasliwal et al. 2017; Xie et al. 2018)

$$\rho(t, \theta) = \begin{cases} \rho_{\rm ej} \left(\frac{1}{4} + \sin^3 \theta\right), & t < 5 \text{ ms}, \\ \rho_{\rm ej} \left(\frac{t}{5 \text{ ms}}\right)^{-2} \left(\frac{1}{4} + \sin^3 \theta\right), & 5 \text{ ms} < t < 15 \text{ ms}, \end{cases}$$

$$\tag{1}$$

where θ is the polar angle measured from the jet axis, and ρ_{ej} is solved from the ejecta mass (M_{ej}) by

 $\int_0^{15 \text{ ms}} \rho(t, \theta) v_{\rm ej} r_{\rm in}^2 dt d\Omega = M_{\rm ej}.$ Similar to other works, the inner boundary of the simulation domain $r_{\rm in}$ is set to be $5 \times 10^7 \text{ cm}$, and $M_{\rm ej} = 10^{-2} M_{\odot}$ is adopted.

2.2. The Jet

As we mainly focus on the jet propagation, in our simulations a relativistic jet is produced via a set of boundary conditions without including the detailed jet-launching mechanism. We consider a stable, hot magnetic jet, of which the transversal equilibrium between the total pressure gradient, the centrifugal force, and the magnetic tension is already established. The jet material at the inlet is characterized by eight angular functions, namely density (ρ_j) and pressure (p_j) in the fluid frame, velocities in three directions $(v_j^r, v_j^{\theta}, v_j^{\phi})$, and magnetic field in the laboratory frame $(B^r, B^{\theta}, B^{\phi})$. These functions are determined as follows.

From an observational point of view, a jet is described by its luminosity (L_j) and the terminal Lorentz factor Γ_{∞} . The specific gas enthalpy of the jet material is given by

$$h = 1 + \frac{1}{\rho_i c^2} (\langle e_j \rangle + \langle p_j \rangle) = 1 + \frac{4 \langle p_j \rangle}{\rho_j c^2}, \tag{2}$$

where e_j is the internal energy density, and we have taken the adiabatic index as 4/3 ($e_j = 3p_j$). The brackets in Equation (2) denote the average values across the half-opening angle of the jet θ_j . Defining two magnetization parameters as⁶

$$\sigma_{\phi} \simeq \frac{\langle (b^{\phi})^2 \rangle}{2 \langle p_j \rangle}, \ \sigma_r \simeq \frac{(B^r)^2}{2 \langle p_j \rangle},$$
(3)

where $(b^{\phi})^2$ is the energy density of the azimuthal magnetic field in the fluid frame, one can then define the specific enthalpy including the contribution of the magnetic field as

$$h^{*} = 1 + \frac{1}{\rho_{j}c^{2}}(\langle e_{j} \rangle + \langle p_{j} \rangle) + \frac{b^{2}}{\rho_{j}c^{2}}$$

= $h + \frac{1}{2}(h - 1)(\sigma_{r} + \sigma_{\phi}).$ (4)

When the internal energy and the magnetic energy in the jet are fully converted to kinetic energy, the jet material would reach a terminal Lorentz factor Γ_{∞} , which is calculated as $\Gamma_{\infty} \sim \Gamma_r \times h^*$ (Γ_r is the initial Lorentz factor of the radial direction). On the other hand, the energy density in the lab frame can be expressed as $e_{\text{lab}} = \Gamma_r^2 h^* \rho_j c^2$, which is related to L_j by

$$L_j = 4\pi r_{\rm in}^2 v_j^r e_{\rm lab}.$$
 (5)

For simplicity, we use a top-hat profile for all three parameters ρ_j , v_j^r and B^r , which means that they are constant within θ_j . Thus, ρ_j could be obtained from Equation (5) under specific values of L_i , Γ_{∞} , and v_i^r .

⁶ Notice that here we adopt a more generalized definition of σ by taking the enthalpy rather than the rest mass density in the denominator. Note that the total co-moving magnetic energy density can be written as $b^{2} = b^{\mu}b_{\mu} = \frac{B^{2}}{\Gamma^{2}} + (\mathbf{v} \cdot \mathbf{B})^{2} \approx \frac{(B^{r})^{2} + (B^{\phi})^{2}}{\Gamma_{r}^{2}} + (B^{r} \cdot v_{j}^{r})^{2} = (B^{r})^{2} + \frac{(b^{\phi})^{2}}{\Gamma_{r}^{2}} = (B^{r})^{2} + (b^{\phi})^{2} \quad \text{when} \quad B^{\theta} = v_{j}^{\theta} = 0 \quad \text{and} \quad v_{j}^{\phi} < v_{j}^{r} \ (\Gamma \approx \Gamma_{r} = 1/\sqrt{1 - (v_{j}^{r})^{2}}).$

							4
Jet Scenario	$\Delta t_{\rm jet}$	$ heta_j$	Luminosity (L_j)	Γ_{∞}	v'_j	B'	$B_{j,m}^{\phi}$
	(s)		(erg s ⁻¹)		(<i>c</i>)	(G)	(G)
M0.01	0.01	10°	5×10^{51}	265	0.8	3.1×10^{12}	6.2×10^{12}
M0.1	0.1	10°	5×10^{51}	265	0.8	3.1×10^{12}	6.2×10^{12}
M0.5	0.5	10°	5×10^{51}	265	0.8	3.1×10^{12}	6.2×10^{12}
M1.0	1.0	10°	5×10^{51}	265	0.8	3.1×10^{12}	6.2×10^{12}

 Table 1

 Initial Conditions of the Jet Scenarios

For the azimuthal magnetic field we adopt a profile as (also see Martí 2015)

$$B^{\phi}(\theta) = \begin{cases} \frac{2B_{j,m}^{\phi}(\theta/\theta_m)}{1+(\theta/\theta_m)^2}, & 0 < \theta < \theta_j, \\ 0, & \theta > \theta_j, \end{cases}$$
(6)

where the azimuthal magnetic field increases linearly for $\theta \ll \theta_m$, reaching a maximum $(B_{j,m}^{\phi})$ at θ_m and decreasing as $1/\theta_j$ for $\theta > \theta_m$. A moderate value for θ_m/θ_j , 0.4, is adopted as a typical magnetic profile. Because the central engine of a short GRB is believed to be rapidly rotating, the jet is assumed to be in rigid rotation, i.e.,

$$v_i^{\phi}(\theta) = v_{i,m}^{\phi}(\theta / \theta_j), \ 0 < \theta < \theta_j.$$
(7)

In the following simulations, $v_{j,m}^{\phi}$ is set to be 0.4*c*, which is the equivalent of having a central engine with a rotating period of ~5 ms at the inner boundary of the jet; v_j^{θ} and B^{θ} are set to be zero as they are usually much smaller than other components of an RMHD jet at the inlet. Combining Equations (3) and (6)–(7) we then solve the transversal equilibrium equation (see Martí 2015)

$$\frac{dp_j}{d\theta} = -\frac{(B^{\phi})^2}{\theta(\Gamma^r)^2} - \left(\frac{B^{\phi}}{(\Gamma^r)^2} + B^r v_j^r v_j^{\phi}\right) \frac{dB^{\phi}}{d\theta}
+ (B^r v_j^{\phi} - v_j^r B^{\phi}) B^r \frac{dv_j^{\phi}}{d\theta} + \frac{\rho_j h \Gamma^2 (v_j^{\phi})^2}{\theta}
+ \frac{B^r v_j^{\phi}}{\theta} (B^r v_j^{\phi} - 2B^{\phi} v_j^r)$$
(8)

to obtain p_j with specific B^r and $B_{j,m}^{\phi}$. In practice, B^r and $B_{j,m}^{\phi}$ are fixed to meet the conditions of σ_r and σ_{ϕ} through several trials.

The magnetization of the GRB jet is still under debate. The initial magnetization may be high (≥ 100) in the vicinity of the central engine. On the other hand, dissipation processes may convert a significant fraction of the magnetic energy into the internal energy soon after launch (Bromberg & Tchekhovskoy 2016). In this Letter, we choose an equipartition case, i.e., $\sigma_r \sim \sigma_\phi \sim 1$ in the simulations.

After the NS merger, the jet launching may be delayed by a duration of Δt_{jet} in comparison with the start time of ejecta. The value of Δt_{jet} depends on the type of the central engine and the jet-launching mechanism of GRBs. In general, Δt_{jet} should consist of the timescale to establish either an accretion disk or strong magnetic fields, and the timescale to launch a relativistic jet when mass loading is low enough. It may range from 10 ms to several seconds (see Zhang 2019 for details). In our simulations, we investigate four representative values of Δt_{jet} : 0.01 s, 0.1 s, 0.5 s, and 1.0 s. The jet scenarios are named using

the form of "Mi," $i = \Delta t_{jet}$. We have chosen the same values of θ_j , L_j , Γ_{∞} , and v_j^r for these four cases to isolate the effect of Δt_{jet} . All of the initial parameters of the four scenarios are listed in Table 1. The jet angle θ_j is taken to be 10°, which is roughly a median jet opening angle for short GRBs (Fong et al. 2015; Beniamini et al. 2019). Typical values of $L_j = 5 \times 10^{51} \,\mathrm{erg \, s^{-1}}$ (Guetta & Piran 2005) and $\Gamma_{\infty} \sim 300$ are adopted. In Table 1, one can see $B^r \sim B_{j,m}^{\phi} \sim 10^{12} \,\mathrm{G}$ at r_{in} . This corresponds to a magnetic strength of $10^{14} \,\mathrm{G}$ at $10^6 \,\mathrm{cm}$ (the surface of a central object), and is consistent with that invoked in previous jet-launching theories (e.g., Blandford & Znajek 1977).

2.3. Method

We run axisymmetric and midplane symmetric 2.5D RMHD simulations using the PLUTO code (version 4.2, see Mignone et al. 2007 for a full description). Spherical coordinates (r, θ) are employed and axisymmetry is assumed for all the simulations. The computational domain covers a region of $r_{in} \leq r \leq 6 \times 10^{10}$ cm and $0^{\circ} \leq \theta \leq 90^{\circ}$. The radial grid consists of 2312 points and is logarithmically distributed, while the angular grid is uniform with 512 points, making the cell aspect ratio ~1. With this setup, the jet is resolved by roughly 60 cells across θ_{j} , comparable to previous 2D studies. A Riemann solver called the HLLD solver (see Miyoshi & Kusano 2005; Mignone et al. 2009, 2010), a linear-type spatial reconstruction, and a second-order Runge–Kutta time integration were chosen in the simulations. As a result, we achieve second-order accuracy in both space and time.

3. Simulation Results

Before the jet launching, the dynamical ejecta is injected as shown in Section 2.1. After Δt_{iet} , the jet material is injected as described in Section 2.2. We have simulated four jets with the delay time of $\Delta t_{\text{jet}} = 0.01 \text{ s}, 0.1 \text{ s}, 0.5 \text{ s}, \text{ and } 1.0 \text{ s}, \text{ respectively.}$ The total duration of the jet is 1.0 s for all cases. In Figure 1, we show the distributions of density and Γ at the time when the jet has been launched for 0.5 s, i.e., half of the total duration. Similar to pure hydrodynamical simulations, a cocoon emerges to generate the pressure needed to counterbalance the pressure from the surrounding ejecta. It is seen that the interaction between the jet and the cocoon is weaker for a smaller Δt_{iet} because the jet funnel is formed quickly, which leads to a higher Γ for materials beyond the θ_j . After the breakout, the Lorentz factor of the jet core accelerates linearly with r, while the Lorentz factor beyond the jet core becomes angle dependent, together with the expansion of the cocoon material.

The breakout time of the hot magnetic jet, t_{bo} , for each simulation is presented in Figure 2. Assigning the average velocity of the jet head before breakout as v_{hj} , the jet breakout



Figure 1. Lorentz factor map and density distribution (in units of g cm⁻³) of four scenarios (with different Δt_{jet}) when the jet material has been ejected for a period of 0.5 s. Blue lines depict the magnetic field lines on the *X*-*Y* plane. The unit scale for *X* and *Y* axis is 10⁷ cm.



Figure 2. Relation between the breakout time of the jet and Δt_{jet} for our simulation results. The shadow area shows the analytic results when the jet head velocity is in the range of 0.3–0.4*c*.

time since the merger can be estimated as

$$t_{\rm bo} = \Delta t_{\rm jet} + \frac{v_{\rm ej} \Delta t_{\rm jet}}{v_{\rm ih} - v_{\rm ej}}.$$
(9)

As shown in Figure 2, t_{bo} obtained from the simulation results is well consistent with that derived from Equation (9) when v_{jh} is within the range of 0.3c-0.4c.

From these simulations, we investigate the relationship between Δt_{jet} and the structure of the jet. The jet is quenched artificially at the inner boundary after being launched for 1 s. When the last injected jet material has escaped from the outer edge of the ejecta, we can calculate the equivalent Lorentz factor averaged along the radial direction as an estimate for the terminal Lorentz factor of the outflow, i.e.,

$$\bar{\Gamma}(\theta) = \left(\frac{\int_{r_{\text{out}}} \Gamma^2(\rho c^2 + 4p + b^2) \, dV}{\int \rho c^2 \, dV}\right)^{1/2},\tag{10}$$

where r_{out} is the radius of the outer edge of the ejecta. One could compare the equivalent Lorentz factor for each case in a straightforward view rather than a 2D view in Figure 1.



Figure 3. Angular distribution of $\overline{\Gamma}\overline{\beta}$ of the outflow for the four cases after the jet escapes from the outer edge of the ejecta. The position of initial θ_j is marked by the vertical dashed line.

Similarly, one could derive the outflow energy per solid angle by integrating energy along the radial direction

$$\frac{dE}{d\Omega} = \frac{\int_{r_{\text{out}}} \Gamma^2(\rho c^2 + 4p + b^2) \, dV}{2\pi \sin \theta d\theta}.$$
(11)

The jet $\overline{\Gamma}\overline{\beta}$ and energy angular structure for the four jets are presented in Figures 3 and 4, respectively. One can draw the following interesting conclusions. First, regardless of Δt_{jet} , an angular structure is always formed for both $\overline{\Gamma}\overline{\beta}$ and $dE/d\Omega$. At the viewing angle θ_{v} , which is several times of the jet opening angle θ_i , there is always mildly relativistic ejecta moving along the line of sight. The case of GW170817/GRB 170817A is therefore naturally expected. Second, for a relatively small Δt_{jet} , e.g., 0.01 and 0.1 s, the material beyond the initial jet opening angle (10°) is significantly faster than the case of a large Δt_{iet} , e.g., 0.5 and 1 s. This is because the jet very quickly breaks out from the ejecta and subsequently forms an angular structure. The line-of-sight material is dominated by the jet material. Finally, for a relatively large Δt_{jet} , e.g., 0.5 and 1 s, $dE/d\Omega$ at a large viewing angle is large compared with the case of a small Δt_{jet} , e.g., 0.01 and 0.1 s. This, combined with a relatively small $\overline{\Gamma}\overline{\beta}$, indicates significant mass loading. The line-of-sight material at a relatively large θ_v is dominated by the cocoon material. In general, the cocoon emission becomes progressively important as Δt_{iet} becomes larger; for example, longer than 0.5 s.

4. The Case of GW170817/GRB 170817A

The first NS–NS merger GW event GW170817 was associated with a low-luminosity short GRB 170817A. There are several open questions related to the physics of short GRB 170817A. (1.) There was a $\Delta t \sim 1.7$ s delay of GRB 170817A with respect to GW170817. What is the origin of the delay? (2.) The afterglow and prompt emission data are consistent with a structured jet. What is the origin of the jet structure? In particular, is the mildly relativistic material along the line of sight from the cocoon, or the wing of a structured jet? (3.) What is the radiation mechanism of the γ -rays, thermal emission from the photosphere, or synchrotron radiation? (4.) What is the



Figure 4. Angular distribution of the total energy per solid angle of the outflow for the four cases.

central engine of GRB 170817A, a BH formed after a brief hypermassive NS phase or a long-lived NS?

The current available data are not enough to fully address these open questions. Our simulations shed light on to some of these problems. According to our simulations, there could be two scenarios to account for the data in principle.

The first scenario, which has been discussed in the literature (e.g., Nakar et al. 2018), interprets the prompt emission as the thermal emission of the cocoon material at shock breakout. This scenario corresponds to the case of a relatively long Δt_{jet} (e.g., our M0.5 and M1.0 scenarios). In this model, because the jet launching is delayed, the cocoon emission is significant. Within this scenario, the delay time between the jet breakout and emission is

$$\delta t_R \sim R_{\rm GRB} / 2\Gamma^2 c \approx 0.7 \, {\rm s} \left(\frac{R_{\rm GRB}}{10^{12} \, {\rm cm}}\right) \left(\frac{\Gamma}{5}\right)^{-2},$$
 (12)

which is smaller than the observed 1.7 s delay. One needs to attribute the most delay time to t_{bo} , which is consistent with the requirement of a significant Δt_{jet} . Meng et al. (2018) showed that the thermal radiation from a structured jet can account for the observed GRB spectrum. Within this scenario, one has to explain why Δt_{iet} is significantly longer than the dynamical timescale of the central engine (~millisecond). One possibility is that this timescale is the existence timescale of the hypermassive NS, and the jet launching happened after the collapse of the NS. This hypermassive NS phase seems to be favored for interpreting the kilonova data (Margalit & Metzger 2017). On the other hand, there is no obvious reason why a relativistic jet cannot be launched during the hypermassive NS phase. Another issue of this interpretation is that the observed duration of the short GRB is much longer than $\delta t_{\rm R}$, which defines the typical duration of a shock breakout GRB through the angular-spreading timescale. One needs an additional mechanism to interpret the duration.

The second mechanism interprets γ -ray emission as synchrotron radiation in an optically thin region well beyond the photosphere radius. The thermal emission is suppressed because the jet is Poynting-flux dominated (Zhang & Yan 2011). Within this scenario, R_{GRB} and Γ are not specified,

but the parameter $\delta t_R \sim R_{\rm GRB}/2\Gamma^2 c$ (which depends on both $R_{\rm GRB}$ and Γ) is set to a value ~ 2 s, which is consistent with both the delay time and the duration of the GRB (Zhang et al. 2018). Within this scenario, $\Delta t_{\text{jet}} \ll \Delta t$, so that the cocoon emission is not significant. The line-of-sight emission is dominated by the wing of the structured jet after the breakout time. Meng et al. (2018) showed that synchrotron radiation from a large emission radius (Uhm & Zhang 2014; Burgess et al. 2018) can also interpret the data well. The broadband afterglow emission is also consistent with such a structured jet model (e.g., Lazzati et al. 2018; Troja et al. 2018; Piro et al. 2019). Within this scenario, a relativistic jet is launched shortly after the merger, within several dynamical timescales, regardless of the central engine of the short GRB. A BH may be formed, but not required. A long-lived NS can also be the engine of GRB 170817A, as suggested by several authors (e.g., Ai et al. 2018; Geng et al. 2018; Li et al. 2018; Yu et al. 2018; Piro et al. 2019).

5. Conclusions

In this Letter, we have performed a series of 2.5D simulations of the propagation of a hot magnetic jet in the dynamical ejecta of a binary NS merger. The effect of the time delay between the merger time and the jet-launching time has been investigated. Regardless of Δt_{jet} , a structured jet with an angle-dependent energy and Lorentz factor is formed after breakout. The angular distribution of $\bar{\Gamma}\bar{\beta}$ and $dE/d\Omega$ show that for a relatively small Δt_{jet} , the ejecta along the direction of θ_{ν} greater than θ_j is dominated by the jet itself in a low-luminosity, low- Γ wing. For a relatively large Δt_{jet} , e.g., 0.5 s and longer, the large viewing angle direction is dominated by a mildly relativistic cocoon.

Our results suggest that the observed ~ 1.7 s delay between GRB 170817A and the merger time of GW170817 could be explained by either synchrotron scenario with a negligible $\Delta t_{\rm iet}$, or by the photosphere scenario with a relatively large Δt_{jet} . Whether the line-of-sight emission is from the wing of a structured jet or the cocoon material depends on Δt_{iet} . The data of GW170817/GRB 170817A cannot differentiate between the two scenarios. However, future more GW/GRB associations for NS-NS mergers can help to solve the problem. In particular, the synchrotron scenario requires that the observed delay timescale is comparable to the duration of the burst, while the cocoon scenario interprets the delay timescale and duration with different mechanisms so that the two timescales, in principle, can be very different. Accurate constraints on the jet components and emission radius (e.g., Matsumoto et al. 2019) provide another way to differentiate between these two scenarios.

In contrast with the simulations of a pure hydrodynamic jet $(\sigma = 0, \text{ e.g.}, \text{Lazzati et al. 2017}; \text{Xie et al. 2018})$ or a Poyntingflux dominated jet $(\sigma \ge 1, \text{ e.g.}, \text{Bromberg et al. 2018})$, we have focused on the hot magnetic jet with $\sigma \sim 1$ in this work. A more realistic investigation of the jet structure should include both the jet-launching mechanism (Kathirgamaraju et al. 2019), the energy dissipation within the jet, and its propagation in the ejecta. Furthermore, radiation transfer should be properly implemented in RMHD simulations to directly relate jet simulations to GRB prompt emission. All of these will be considered in further studies.

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